

# i-Capacitor Voltage Control for PV Z-source System with Enhanced Shoot-through

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## ABSTRACT

This paper explains an improved capacitor voltage control (i-CVC) by combining with maximum power point tracking (MPPT) algorithm as a control strategy for a single-phase Z-source inverter (ZSI) using photovoltaic (PV) source. The existing CVC based-MPPT control algorithm has a net shoot-through interval which should be inserted in the switching waveforms of the inverter to produce maximum power at the Z-network of the PV. However, this net shoot-through period is formed by an additional shoot-through period which has drawbacks as it boosts the capacitor voltage to a greater extent beyond the allowable voltage boundary of the capacitor. In other words, the PV will boost the voltage more than the desired level as per required by reference capacitor voltage of the Z-network. Due to this problem, an improved capacitor voltage control (i-CVC) with general Perturb and Observe (P&O) based on  $\Delta T_0$  configuration of the changes shoot-through duty cycle to maintain the DC-link of the ZSI is introduced and been tested in simulation case with a resistive load. At the end, this modification able to assist the MPPT output power by increasing the overall system effectiveness of power generation by the PV.

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## 1. INTRODUCTION

Solar power generation is one of guarantee free electrical generation today. Therefore, it has an abundant power that needs to be harvest continuously. In order to harvest this energy, a power conditioning system for PV is needed, by applying two stages converter topologies [1]. The first stage is, to boost the PV output voltage to the desired level before it can be converted to AC signal for AC source applications using the inverter at the second stage [2], [3]. This strategy requires two converters, controllers and feedback responses. As a solution, a single-stage Z-source inverter (ZSI) based on one power circuitry generation has been proposed to overcome these drawbacks appeared in the common voltage and current source inverter based on [4].

Block diagram of the improved ZSI with a unique impedance network is shown in Figure 1. As been compared in many literature studies on the ZSI, a DC-AC inversion for PV have been carried out due to their advantages such as, it used less number of components, reduce overall cost of development from harvesting the sunlight to electrical output, and enlarges its application [5], [6]. If this topology needs to be implemented in PV generation, a modification is necessary in MPPT controller in order to maintain the DC-link voltage, protect the PV module on reverse current and able to maintain the supply even after the irradiation of PV is changed without using boost converter. Some researchers have used the soft-computing technique combines with the conventional methods [7], [8] in order to have good MPPT power as well as be able to maintain the



capacitor voltage at the Z-circuitry. However, the soft-computing approach causes the system effectiveness to be reduced and give a high cost of construction.

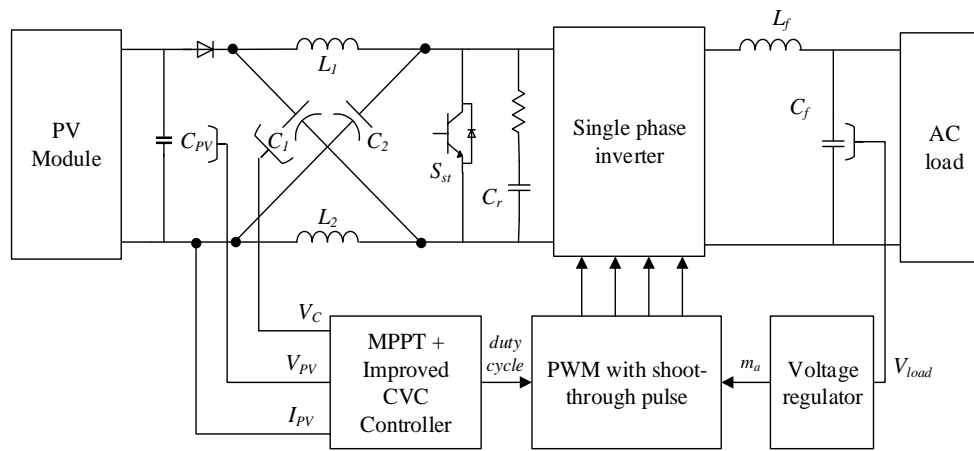


Figure 1. The proposed Control Scheme for Z-source Inverter Based PV Power Conversion System

Since all the MPPT algorithms in ZSI requires to generate a shoot-through period to extract maximum power from solar PV, this shoot through period is unable to boost the capacitor voltage at the impedance network more than the required level. Therefore, this capacitor voltage control (CVC) for ZSI is getting a lot of attention by researchers to be carried out recently. For example, a suggested controller such as traditional MPPT controller with DC-link control is needed in order to produce an additional shoot-through duty ratio and to improve the response time of MPPT controllers as have been proposed in [9], [10]. Papers [11] have proposed a unified MPPT control strategy for ZSI based on PV system to achieve MPPT as well as Z-source capacitor voltage control at the meantime. A modified Perturb and Observe (P&O) technique has been used for the MPPT control and the CVC as the additional controller. This modified conventional algorithms are simpler, less complex and require less parameter [12] that makes this MPPT can be implemented easily into ZSI.

There are three main factors that affect the efficiencies of a PV plant which are the inverter efficiency, MPPT efficiency and PV plant efficiency. The existing version of CVC is employed to the MPPT shoot-through interval,  $T_0$  for obtaining the total shoot-through states,  $T_{sh}$ . The P&O has been used as the MPPT to generate the minimum shoot-through period,  $T_0$  in order to extract maximum power point voltage from the PV module. The extra shoot-through period,  $T_0'$  is generated by the capacitor voltage control (CVC) algorithm is required to increase the Z-network capacitor voltage at the PV panel. Then, the extra shoot-through period,  $T_0'$  is added to the MPPT generated shoot-through interval,  $T_0$  in order to obtain the total shoot-through states,  $T_{sh}$  as shown in Figure 2(a). However, the existing CVC algorithm, boost the capacitor voltage to a greater extent more than the allowable extra shoot-through state would withstand in which caused the capacitor voltage of Z-source cannot be constantly maintained. As a result, all the system efficiency especially, for the inverter and MPPT efficiency are been affected. Hence, this paper introduces an improved CVC (i-CVC) algorithm by adding  $\mp \sum\%$  of changes ( $\Delta T_0'$ ) in shoot-through duty ratio,  $D_0$  and the additional shoot-through duty ratio,  $D_0'$  in order to increase the efficiency of the whole PV system. The  $D_0$  can be denoted as  $T_0/T$  and  $D_0'$  is equal to  $T_0'/T$  as illustrate in Figure 2(b). Therefore, by adding  $\mp \sum\%$  of  $\Delta T_0'$  to the controller, it can reduce the drawback of the controller performance by achieve a constant capacitor voltage at input of Z-source and a maintained DC-link voltage at the output of ZSI.



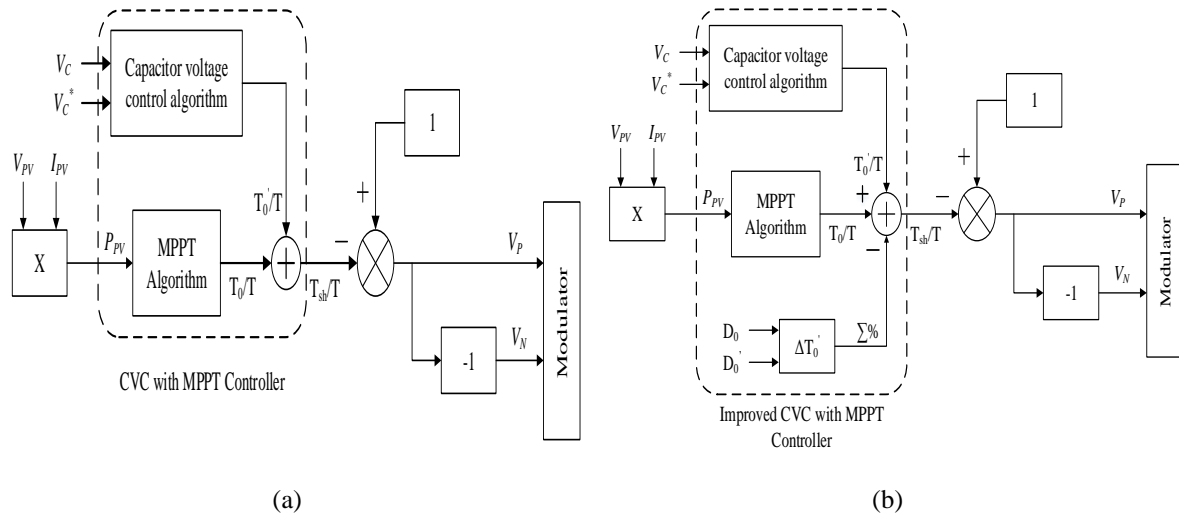


Figure 2. Z-source Inverter PV Power Conditioning System Control Block Diagram (a) Existing CVC Controller (b) Proposed CVC Controller

This paper is organized as follows: Proposed improved CVC algorithm based MPPT in Section 2. The whole system configuration is discussed in Section 3. Section 4 comprised result of simulation and discussion, followed by conclusion part is made in Section 5.

## 2. PROPOSED CAPACITOR VOLTAGE CONTROL (i-CVC) BASED MPPT

In this section, the development of the proposed controller will be discussed. For a solar power generation system, the MPPT and a stable output voltage are two main objectives of the system in order to achieve high efficiency output. Therefore, two control variables are involved in ZSI which is the shoot-through duty ratio and the modulation index as suggested from [13] that need to be considered. Therefore, i-CVC control scheme is introduced in order to achieve both, MPPT and voltage control at Z-network as well by introducing the limiter boundary.

### 2.1. Control Strategy Development

The shoot-through period ( $T_0$ ) is generated by traditional Perturb and Observe (P&O) based on MPPT technique in order to extract maximum power point voltage from PV module [14], [15]. This  $T_0$  is unable to boost the capacitor voltage of Z-network further than the desired level due to the uncontrolled charging and discharging of Z-network impedances. Therefore, a capacitor voltage control of the impedance network is essential in order to control the capacitor voltage beyond the maximum power point voltage. It needs to be calculated using the shoot-through period ( $T_0$ ) that requires to boost the capacitor voltage to the MPP voltage and combines with the additional shoot-through period ( $T_0'$ ) to control the capacitor voltage beyond the MPP voltage.

Unfortunately, the additional shoot-through period ( $T_0'$ ) has some drawbacks as it boosts the capacitor voltage to a greater extent. Figure 3 shows the generation of the proposed controller with simple boost control method with two conditions of boundary of  $\Delta T_0'$  while Fig.4 indicates the control algorithm for P&O based MPPT with embended i-CVC mechanism. It illustrates that, two references straight lines ( $V_p^*$  and  $V_n^*$ ) are continuously regulated to maintain Z-source capacitor voltage.

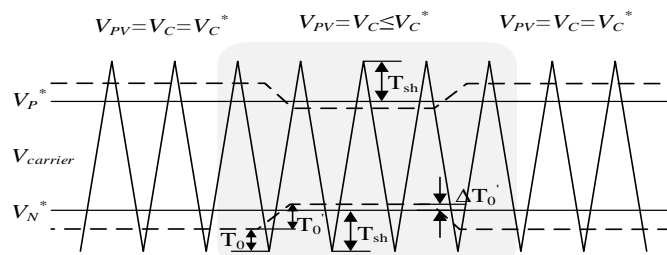


Figure 3. Shoot through generation by improved CVC control strategy



The new shoot-through period ( $T_{sh}$ ) of MPPT control has been synchronized with improved CVC algorithm and can be defined as followed:

$$T_{sh} = T_0 \pm T_0' \mp \sum \% \Delta T_0' \quad (1)$$

$$D_{sh} = \frac{T_{sh}}{T} = \frac{T_0}{T} \pm \frac{T_0'}{T} \mp \sum \% \Delta T_0' \quad (2)$$

where,  $D_{sh}$  can be referred as the total shoot-through duty ratio and is equal to  $T_{sh}/T$ . ( $T_0$ ) is used to track  $V_{PV}^*$  by add or subtract the  $\Delta T_0$  for various climate condition at the PV input, while ( $T_0'$ ) is used to control Z-source capacitor voltage according to reference capacitor voltage,  $V_C^*$ . At the meantime, the additional  $\mp \sum \% \Delta T_0'$  will try to reduce the greater extent voltage occurs while boosting the capacitor voltage at Z-network by ( $T_0'$ ) to the reference value. As the result, the capacitor voltage will be controlled and able to maintain the DC link voltage as well. The range of the new shoot-through time period ( $T_{sh}$ ), can be written as suggested by the authors to:

$$\frac{T_{sh}}{T} \mp \sum \% \Delta T_0' \leq (1 - M), \quad (3)$$

where,  $M$  is the modulation index. From equations (1) and (3) the following modified equation is obtained:

$$\pm \frac{T_0'}{T} \mp \sum \% \Delta T_0' \leq 1 - \left( M + \frac{T_0}{T} \right). \quad (4)$$

Therefore, the maximum value of the additional shoot-through duty ratio for both cases can be written as followed:

$$\left( \frac{T_0'}{T} \mp \sum \% \Delta T_0' \right)_{\max} \leq 1 - \left( M + \frac{T_0}{T} \right) \quad \text{when } V_C^* > V_C, \quad (5)$$

$$\left( \frac{T_0'}{T} \mp \sum \% \Delta T_0' \right)_{\max} \leq - \left( 1 - \left( M + \frac{T_0}{T} \right) \right) \quad \text{when } V_C^* < V_C. \quad (6)$$

Moreover, the modulation index ( $M$ ) and the MPPT shoot-through ratio ( $D_0$ ) is used to limit the range of the additional shoot-through duty ratio ( $D_0'$ ) combines with  $\mp \sum \% \Delta T_0'$  and hence achieve the Z-source capacitor voltage control. Two constant references are employed to realize the new shoot-through period where now be equal to:

$$V_P^* = \left[ 1 - \left( \frac{T_{sh}}{T} \mp \sum \% \Delta T_0' \right) \right] = \left[ 1 - (D_{sh} \mp \sum \% \Delta T_0') \right] \quad (7)$$

$$V_N^* = - \left[ 1 - \left( \frac{T_{sh}}{T} \mp \sum \% \Delta T_0' \right) \right] = -V_P^*. \quad (8)$$

These two equations are compared with high-frequency carrier signal in order to generate the shoot-through pulse. Then, the DC link voltage or the capacitor voltage can be improved until it reaches the MPP voltage of the PV module ( $V_{PV}^*$ ) and thus, able extract a maximum power from PV module. At the meantime, the average DC link voltage of the inverter can be expressed as:

$$\bar{v}_{dc} = V_C = \frac{1 - (D_{sh} \mp \sum \% \Delta T_0')}{1 - 2(D_{sh} \mp \sum \% \Delta T_0')} V_{PV}^*. \quad (9)$$

On the AC side, the output peak voltage from the inverter can be defined as:



$$\hat{v}_{ac} = M \left[ \frac{1 - (D_{sh} \mp \sum \% \Delta T_0')}{1 - 2(D_{sh} \mp \sum \% \Delta T_0')} \right] \frac{V_{PV}^*}{2} = M \frac{\bar{v}_{dc}}{2}. \quad (10)$$

The modulation index can be controlled from zero to  $V_p^*$ . In the meantime, the shoot-through states can be applied to all of the legs simultaneously whenever the triangular carrier signal is higher than the  $V_p^*$  or lower than the  $V_n^*$ . Figure 4 shows P&O based MPPT algorithm with improved CVC algorithm.

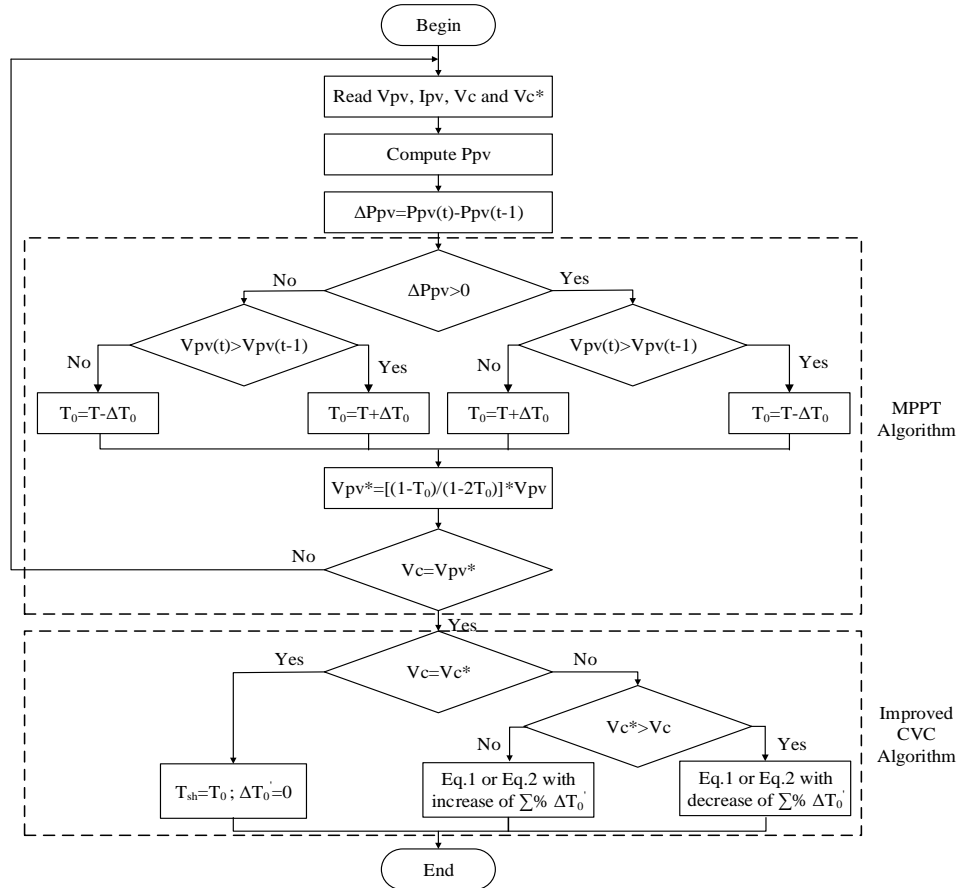


Figure 4. P&O Based MPPT Algorithm with Improved CVC Algorithm

## 2.2. Computation of $\mp \sum \% \Delta T_0'$ in i-CVC Algorithm

In this improved control algorithm, the minimum shoot-through period is required to maintain the Z-source capacitor voltage while the PV voltage at MPP is generated by MPPT algorithm. The general capacitor voltage control (CVC) algorithm is to provide an additional boost in the capacitor voltage while at the same time to track the reference value.

There are three cases in order the capacitor voltage to track the maximum power of PV array where, at first, when the reference capacitor voltage,  $V_c^*$  is equal to the voltage of PV at MPP,  $V_{PV}^*$ . Therefore, only the shoot-through state ( $T_0$ ) is varied to regulate the capacitor voltage while the net shoot-through remains at  $T_0$ . In this case, the shoot-through duty cycle will be set to  $D_0=0.083$ . For the second case, as for example, if  $1000\text{W/m}^2$  and  $25^\circ\text{C}$  irradiant, the voltage delivered by PV panel  $V_{PV}$  is 17V and the maximum power point of the PV panel under this condition is 19V. Now, the shoot-through period generates an extra 2V higher at the Z-source capacitor. The required shoot-through period can be derived from Equation 11 as:

$$v_{dc} = V_c = \frac{1 - D_0}{1 - 2D_0} V_{PV} = V_{PV}^*. \quad (11)$$



This shoot-through period is varied during various irradiant conditions by adding or subtracting the  $\Delta T_0$  and the capacitor voltage boost factor,  $B_c$  can be simplified as followed

$$B_c = \frac{V_{PV}^*}{V_{PV}} = \frac{V_c^*}{V_{PV}}. \quad (12)$$

From Equation 12, the  $B_c$  is calculated to about 1.118 and thus, the shoot-through duty ratio can simply calculate as:

$$D_0 = \frac{T_0}{T} = \frac{B_c - 1}{2B_c - 1}, \quad (13)$$

and give the  $D_0$  equal to 0.095.

For the third case, it is when the capacitor voltage is more than the desired value and beyond the  $V_{PV}^*$  as required in DC link voltage. For example, at  $1000\text{W/m}^2$  and  $25^\circ\text{C}$ , the voltage is delivered by 17V in PV panel and the maximum power point of the PV panel under is targeted value to be 22V. The 22V will be the voltage to maintain the capacitor across the Z-source capacitor. As been detailed in the previous case, the shoot-through time period is to boost the capacitor voltage to this new MPP voltage of PV panel is 0.115. Although, if the additional shoot-through period ( $T_0'$ ) is required for boosting capacitor voltage more than to 22V, it can be calculated using Equations 12 and 13. However, the extra shoot-through duty ratio,  $D_0'$  produces around 0.185 for this case.

In order to increase the efficiency of PV output from the MPPT controller, the suggested improved capacitor voltage control (i-CVC) algorithm must able to handle any values of capacitor voltage at Z-network is employed and suggested. This improved algorithm is able to operate well especially during when, the reference capacitor voltage is lower than the Z-source capacitor voltage. By adding an extra ratio which about  $\mp\sum\%$  of the changes between shoot-through duty cycle for  $D_0$  upon the extra shoot-through duty cycle and  $D_0'$  at the CVC algorithm. It will prove the effectiveness of this algorithm. This percentage has been proved through the calculation in next explanation paragraph.

To verify the application of  $\mp\sum\% \Delta T_0'$ , let the reference capacitor voltage,  $V_c'$  is equal to the voltage of PV at MPP,  $V_{PV}^*$  and the shoot-through duty remains unchanged which is  $D_0=0.083$  as stated earlier in the first case. Then, take the reference capacitor voltage,  $V_c'$  more than to the voltage of PV at MPP,  $V_{PV}^*$ . As known earlier, the maximum reference voltage is set to 22V. Thus, the additional duty cycle requires to boost is  $D_0'=0.185$  and the total shoot-through duty ratio ( $D_{sh}$ ) will regulate to a constant DC input value. However, during the changes between second case and the third case,  $D_{sh}$  has an extra increasing which is more than the desired level. Since that, an additional  $\mp\sum\%$  will be applied to reduce the increment in delta changes of shoot-through over additional shoot-through duty,  $\Delta T_0'$  where  $\Delta T_0'$  given as,

$$\Delta T_0' = \frac{D_0}{D_0'}. \quad (14)$$

By recalculating the required total shoot-through in i-CVC, it is about 10% to 14% of  $\Delta T_0'$  needs to be reduced in order to have a constant capacitor voltage at impedance Z-network. Considering the initial step size,  $\Delta T_0=0.02$ , another 2% off from the required percentage and this makes it becomes 12%. Therefore, the new shoot-through period to be inserted into all the switching waveforms can be derived as in Equation 1 with  $\mp 12\%$  of  $\Delta T_0'$ . The improvement of this algorithm towards capacitor voltage control not only reliable for ZSI implementation, it also will increase the effectiveness of the whole PV system shown in Section 4.

### 3. SYSTEM CONFIGURATION

In this section, the whole system configuration of the proposed control algorithm for ZSI-based PV system will be provided. The PV module is the input to the system while the Z-source inverter is the power converter topology that equippes with an improved MPPT-CVC controller. This controller is used to obtain the voltage respond by the PV module in order to achieve maximum power point. The basic Perturb and Observe (P&O) algorithm for a standalone system [16] is used in ZSI with a combination of Z-source improved capacitor voltage control. At the end, the CVC is able to boost the capacitor voltage at impedance network to be twice is possible or more than the desired level at DC link terminal.



### 3.1. Single-stage PV Conversion System for Z-source Inverter

As known, the PV is a non-linear current-voltage and power-voltage characteristic is continuously varied with temperature and irradiance. The PV model has been developed using the basic circuit equation of the solar cells. Here, the MSX-60 poly-crystalline silicon PV module parameters are used as input into the PV system equations which described the current output of the PV solar. Ideally, continuous varying maximum power point of the solar PV module is being tracked using MPPT control technique.

A Z-source inverter plays an important part in order to increase dc voltage output and as the DC-AC conversion in a single stage that is not available in traditional PV power conditioning system. The ZSI is composed of split-inductors  $L_1$  &  $L_2$  and capacitors  $C_1$  &  $C_2$  which are been connected in cross-shape [17]. The inductors are used to regulate the current ripples and reduces harmonics while the two capacitors are used to regulate voltage ripples and produce pure dc at the inverter input. The ZSI has three operation modes shown in Fig.5: active mode, shoot-through mode, and traditional zero-state mode [18]. During active and zero-state mode, the ZSI operates under the traditional pulse width modulation (PWM) pattern. In the shoot-through mode, the inverter bridge is seen as a short circuit from the DC-link point of view [19].

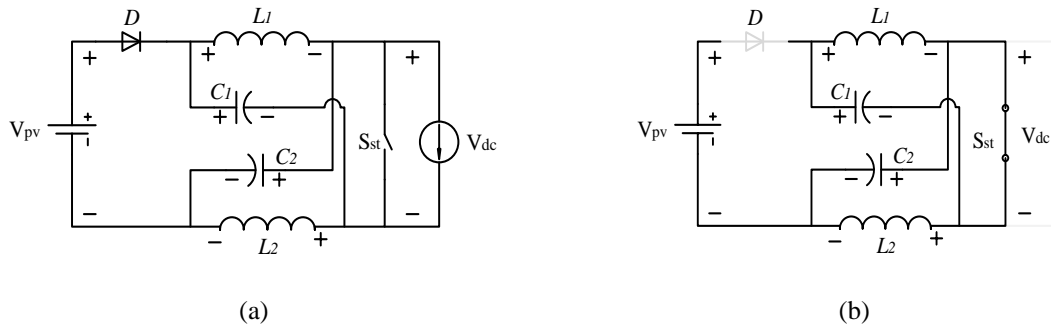


Figure 5. Operating Modes of ZSI. (a) During Non-shoot-through (b) During Shoot-through

Then the DC capacitor voltage can be boosted as,

$$v_{dc} = V_C = \frac{1-D_{sh}}{1-2D_{sh}} V_{PV} = V_{PV}^* \quad (15)$$

$D_{sh}$  is the net shoot-through duty ratio obtained after boosting the capacitor voltage to the desired level.

### 3.2. Selective of Z-network Parameter

The most challenging in designing the ZSI circuitry is the estimation of values for reactive components in impedance network. During the shoot-through time, the Z-source inductor current will discharge the capacitor voltage [20], therefore, the ripple amplitude of the capacitor voltage can be expressed as,

$$\Delta V_C = \frac{D_0 I_L}{f_0 C} \quad (16)$$

and by rearranged equation 16, it gives

$$C = \frac{D_0 I_L}{f_0 \Delta V_C} \quad (17)$$

The maximum current through the inductor occurs when the maximum shoot-through happens. This will cause a high current ripple to the Z-source inductor. In this design, 60% of peak-to-peak current ripple through the Z-network inductor during maximum power operation is been chosen. For the designing of Z-network inductor value, a constant capacitor voltage,  $V_C$  and the ripple current need to be considered. The ripple amplitude of the inductor current is given as,

$$\Delta I_L = \frac{D_0 V_C}{f_0 L} \quad (18)$$



From Equation 18, the inductance can be calculated as

$$L = \frac{D_0 V_C}{f_0 \Delta I_L} . \quad (19)$$

Therefore, all the parameters are being obtained simultaneously. The Z-network inductance,  $L_1=L_2=L=870 \mu\text{H}$  while the for the capacitance,  $C_1=C_2=C=2000 \mu\text{F}$  and capacitive value of PV output voltage,  $C_{PV}=1000 \mu\text{F}$ . Here, the resonant circuit required a resonant capacitance,  $C_r=1000 \mu\text{F}$  with  $10 \Omega$  resistive load. For  $\pm \Sigma\%$  of delta shoot-through,  $\Delta T_0$  required in this simulation test and applicable in this ZSI-PV system is about 12%.

### 3.3. Controller Design Parameter for Voltage Control

As for the bridge inverter control, taking the output voltage of single-phase inverter as a controlled voltage source,  $v_{ac}$  and been combined with the LC filter design to obtain the equivalent circuit as shown in Figure 6.

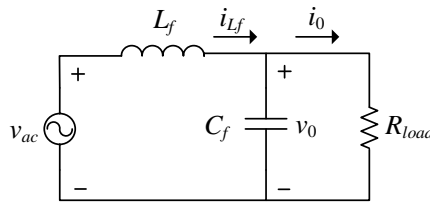


Figure 6. Equivalent circuit of bridge inverter with LC filter

Assume an ideal AC load which is a resistive load  $R$ , then the transfer function of the circuit will be expressed as,

$$G_f(s) = \frac{1}{L_f C_f s^2 + \frac{L_f}{R} s + 1} , \quad (20)$$

which is a typical second-order system. However, from the bode plot in Fig.7(a), shows the design controlled plant of AC inverter output voltage loop is unstable. Therefore, the design of the voltage control loop involves the design of PI controller has been used.

For the voltage control loop, the PI control parameters are designed to get zero-steady state error at the load voltage and 50Hz without affecting the transient response. There are two parameters consist in this section which is the Proportional (P) and the Integral (I). Before the gains of the PI can be selected, the compensating transfer function network by combining  $G_f(s)$  in equation 20 with the ideal compensator of

$$G_{PI}(s) = K_P + \frac{K_I}{s} , \quad (21)$$

where  $K_P$  is proportional gain and  $K_I$  is the integral gain. Then, the voltage closed-loop control system and its closed-loop transfer function is respectively given as

$$G(s) = G_{PI}(s)G_f(s) . \quad (22)$$

Figure 7 shows the bode plot of voltage control loop transfer function,  $G(s)$  with compensator and without the compensator been adding to the plant. By adjusting the gain of the PI regulator, the suitable values for proportional gain,  $K_P=0.575$  and integral gain,  $K_I=0.001$  are obtained from Fig.7(b). It can be seen that, the phase margin of the  $G_f(s)$  is increased to  $90^\circ$  after the compensation, which indicates a stable feature of the closed-loop system.



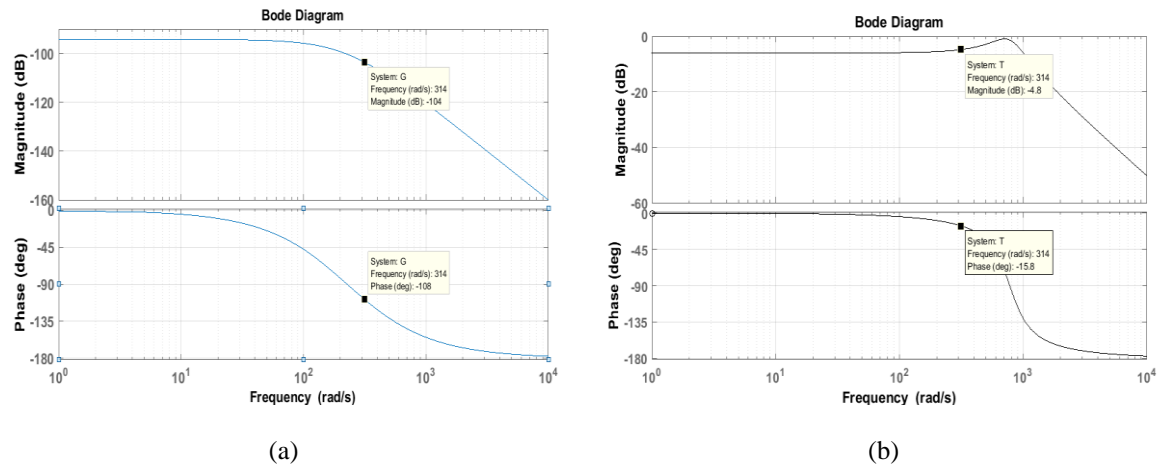


Figure 7. Bode Plots of the Voltage Control Loop (a) Controlled Plant Before Compensation (b) Controlled Plant After Compensation

### 3.4. Pulse Width Modulation (PWM) Control Generation based on i-CVC

The shoot-through state can be applied in conventional PWM in order to make the resonant switch is ON simultaneously during two switches in the same legs. A modified PWM strategy is implemented, which will ensure a single power device switching per state transition. One of the methods in order to generate PWM signal is by using sinusoidal PWM [21], [22] combining with the i-CVC as shown in Figure 8.

In addition, a gate signal is necessary for the complement of a shoot-through signal to improve the switching pattern in ZSI. A quasi-resonant Z-source inverter is formed by adding a quasi-resonant network with only one auxiliary switch connected in parallel between Z-network and the inverter. All switches in the inverter are turned on and off under a zero-voltage switching condition. This topology for ZSI had almost a 10% overall efficiency increase compared with the hard switching. Therefore, this high-performance structure can eliminate the possibility of the DC-link voltage drop with an additional advantage of being stable for all ranges of the modulation index during shoot through state.

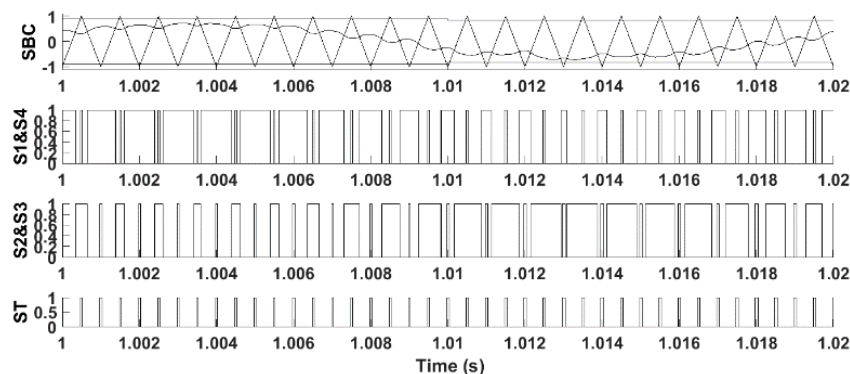


Figure 8. The modified PWM and switching state of ZSI

## 4. RESULT AND DISCUSSION

In this part, the proposed algorithm has been validated through simulation tests using MATLAB/Simulink tools. The simulation model shows exactly how by implementing of  $\Delta T_o$  in duty cycle in additional shoot through will affect the PV system efficiency in term of voltage and power output. There are two different cases or condition of irradiation have been tested in order to see the effectiveness of the algorithm. Firstly, by considering a constantly changes in irradiation and for the second case is when the irradiation is suddenly dropped at a specific time. The simulation time duration of simulations has been set up to 2s whereas some figures have been zoomed in order to have a clear visualization of signals during the changes of irradiation and the DC and inverter outputs performance. In this simulation, the PV module is simulated for a different irradiance but with a constant temperature of 25°C.

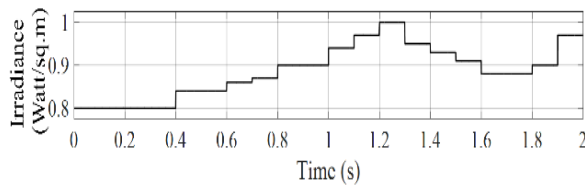


#### 4.1. Case I: Constantly Change in the Irradiation

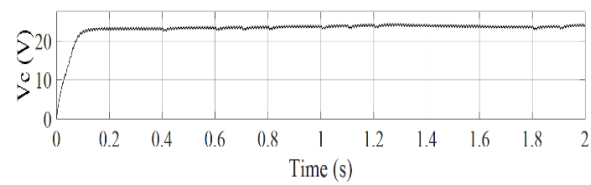
Initially, the PV module is simulated using a constant change of irradiances as designed in Figure 9(a) while Figure 9(b) shows the PV output has been maintained as suggested by authors. As can be seen in Figure 10(a), whenever the constant changes occur, the improved MPPT-CVC voltage of PV module is able to have a constant capacitor voltage for the Z-source. For example, at 0.4s until 1.2s the irradiance is increased constantly until it reaches to the maximum reference voltage, while the capacitor in Z-network, is able to maintain at  $V_C=22V$  at  $S=1000W/m^2$ . After that, the module's irradiance is given by slightly decreased to  $900W/m^2$  from 1.2 to 1.8s in the simulation. It shows that the improved algorithm on i-CVC seems to have ability to control the voltage at impedance network circuitry to be constant as well as the voltage across inverter's DC link terminal voltage in Figure 10(b).

Based on the result, it indicates that the capacitor voltage control with an auxiliary switch is able reduced relatively high fluctuations in order to track maximum power point. This improved controller with additional switch has a better performance as it able to suppress the capacitor voltage ripple too. Due to the constant capacitor voltage at any conditions of solar irradiance, this proposed i-CVC algorithm with the help of additional switch to the system is preferred.

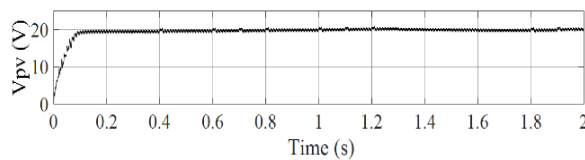
At the meantime, Figure 11 shows the inverter output voltage is regulated to almost 20V as adequate to provide 20V output and output current of 2A respectively with a resistive load of 10 ohms. It indicates that the obtained the gains for PI controller from the bode plot technique manage to ensure the filter output voltage to follow the reference target value.



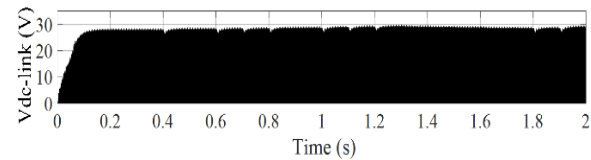
(a)



(a)



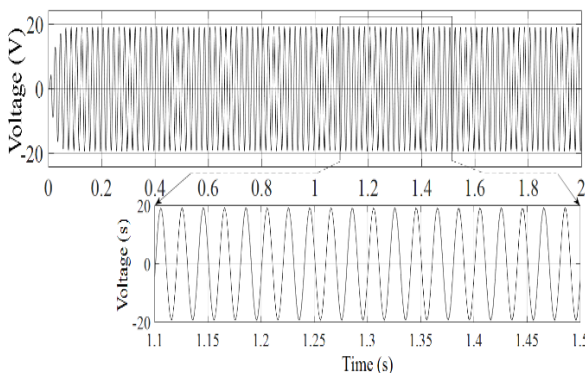
(b)



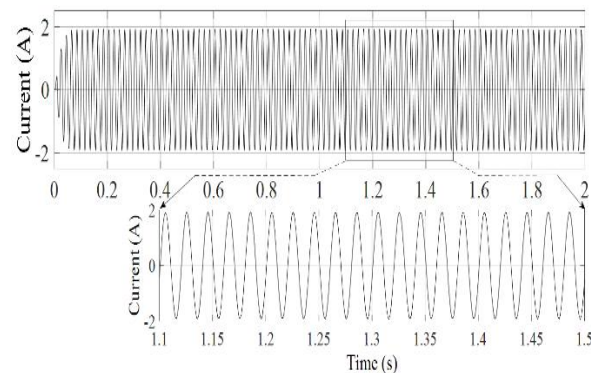
(b)

Figure 9. Input of ZSI for Case 1 (a) Constantly Changes Irradiation at PV (b) PV Output Voltage During Constantly Changing Irradiation

Figure 10. Output of ZSI for Case 1 (a) Capacitor Voltage and, (b) DC-link Voltage at Z-network During Constantly Changing Irradiation



(a)



(b)

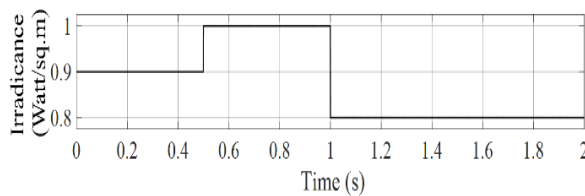
Figure 11. Output Voltage Filter During Constantly Changing Irradiation (a) AC Output Voltage (b) AC Output Current



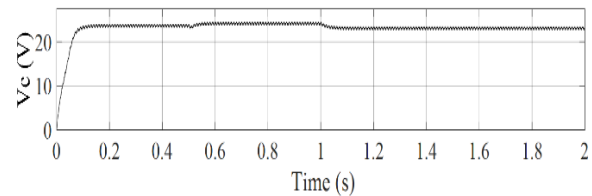
#### 4.2. Case II: Sudden Changes in the Irradiation

Similar to the case I, but for this simulation, a sudden change of irradiance as shown in Figure 12(a) while Figure 12(b) the output PV has been applied using the i-CVC in order to verify the efficiency of the proposed algorithm. Figure 13 shows the performance of capacitor voltage control in order to maintain the Z-network capacitor voltage and the DC link voltage at the same time. The same response for the case I is obtained when the irradiance is changed slowly at time 0.5s. During 1 to 2s of simulation time, the module is working at  $800\text{W/m}^2$ , then a suddenly drop and this cause a small decrease in the capacitor voltage shown in Figure 13(a).

From the aforementioned, the proposed i-CVC algorithm verifies that the additional delta changes about  $\pm 12\%$  in the extra shoot-through duty ratio able to maintain the capacitor voltage at Z-network. Clearly, it proves that, when there is changed of irradiation, the PV module output voltage is still working at the MPP voltage, and the shoot through duty ratio is automatically regulated to keep the peak DC-link voltage to be consistent as in Fig.13(b). It produces an additional boost in capacitor voltage to track the given reference value. Same output performances for the voltage and current after the inverter as in the case 1. The PI control strategy is able to track the given reference voltage even after there is rapidly changing of irradiation.

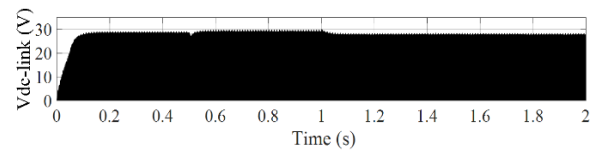


(a)

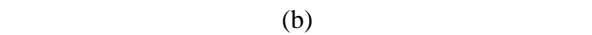


(b)

Figure 12. Input of ZSI for Case 2 (a) Suddenly Changes Irradiation at PV (b) PV Output Voltage During Suddenly Changing Irradiation



(a)



(b)

Figure 13. Output of ZSI for Case 2 (a) Capacitor Voltage and, (b) DC-link Voltage at Z-network During Suddenly Changing Irradiation

#### 4.3. Comparison Between Existing CVC with Improved CVC

Figure 14 shows the comparison performance of capacitor voltage by using existing CVC and i-CVC. From the results, it can be seen that the proposed controlled capacitor voltage has the ability to track the voltage at MPP faster compared to the existing CVC while having a constant output at ZSI. The capacitor voltage obtained almost 24.5 V which is nearly the given reference capacitor voltage,  $V_C^* = 22\text{ V}$ .

Furthermore, the improved CVC has not only increase the tracking accuracy, but it also has a high tracking speed which is 0.04s faster than the existing CVC. Even so, the PI voltage control also has achieved a good performance for both controllers as shown in Figure 15. The output voltage after the inverter gives almost the same but with some improvement in improved CVC. The total harmonic distortion of the output voltage, THD<sub>v</sub>, by using the improved controller also has been reduced from 1.13% to 0.95% as shown in Figure 16 (a) and (b).

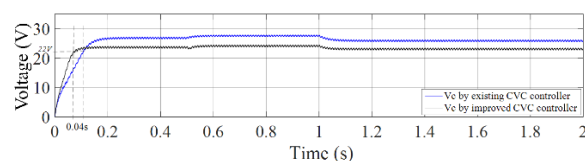


Figure 14. Capacitor voltage by using existing CVC and improved CVC

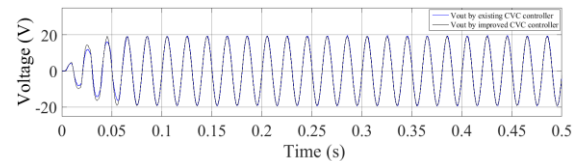


Figure 15. Inverter output voltage by using existing CVC and improved CVC



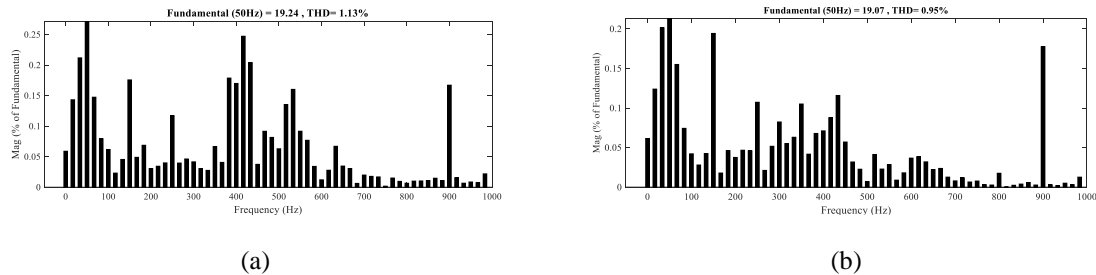


Figure 16. THD<sub>v</sub> of Output Voltage by Using (a) Existing CVC Controller, and (b) Improved CVC Controller

## 5. CONCLUSION

As a conclusion, this paper has introduced an i-CVC algorithm by combining with a conventional MPPT algorithm based on the switching pattern of Z-source inverter with improved shoot through effect. This controller realizes both conditions during varying and sudden changes of irradiation as it can regulate the capacitor voltage at impedance source to be maintained continuously. The effectiveness of the proposed controller has been verified using simulation tests with a well-designed of the control voltage parameter. From the results, the i-CVC with P&O based MPPT method can produce higher tracking accuracy as well as having a fast tracking speed compared to the existing capacitor voltage controller.

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