

Stabilization of the stator and rotor flux linkage of the induction motor in the asynchronous electric drives with frequency regulation

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ABSTRACT

The article is a continuation of the authors' work in research, mainly experimental, asynchronous electric drives with frequency regulation (AED FR) of hoisting-and-transport mechanisms, in which for constructive, operational and other reasons it is difficult to install additional sensors, for example encoders. The results of the analysis of the dynamics of AED FR with two types of sensorless control: vector and scalar are presented in this article. The study was conducted by mathematical modeling in the Simulink application of the MatLab software using standard control system models. The processes of sequential acceleration of the engine to fixed speeds with overload and load shedding on each of them were simulated. At the same time, the speed and effective values of the flux linkages of the rotor and stator and the stator current were monitored, by which the dynamics and efficiency of each type of control were evaluated. As in experimental studies, the dynamic and efficiency of a more stable scalar control was significantly improved by the use of dynamic positive feedback on stator current.

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1. INTRODUCTION

In recent years, a group of engineers at the South Ural State University (SUSU), headed by Prof. Kodkin V.L. has carried out research on the dynamics of asynchronous electric drives with frequency control (AED FC). Operating experience of such drives shows that it is far from always possible to obtain the required static and dynamic characteristics using only standard control algorithms incorporated in the frequency converter. The research directions were formed based on the results of a theoretical analysis of the basic equations of AED FC, but the main results were obtained during experiments and modeling. This is due to the fact that the AED FC equations contain many assumptions and simplifications, the significance of which is very difficult to estimate theoretically.

The results of the experiments are presented in the articles published in Russian and foreign publications [1, 2]. ATV32 and ATV71 frequency converters from Schneider Electric were used as basic equipment. The main result should be considered the worst drive dynamics with sensorless (on speed) vector control as compared with a scalar control drive, containing corrective dynamic positive feedback on the stator current (DPF) [3, 4]. This feedback includes a dynamic link that provides the necessary gain factors for the

To study the scalar control system Figure 2, the model of Professor Louis Desantes (Louis-A. Dessaint) from the state engineering school (École de technologie supérieure) in Montreal (Quebec, Canada) was used [24, 25]. To increase the efficiency of the formation of the electromagnetic torque, positive feedback on the root mean square (rms) value of the stator current was introduced into the control system Figure 3.

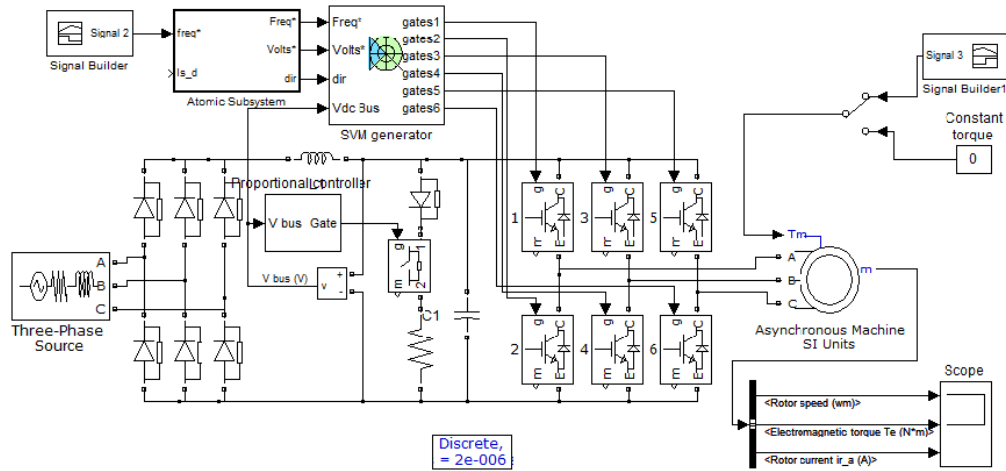


Figure 2. Scheme of scalar control model

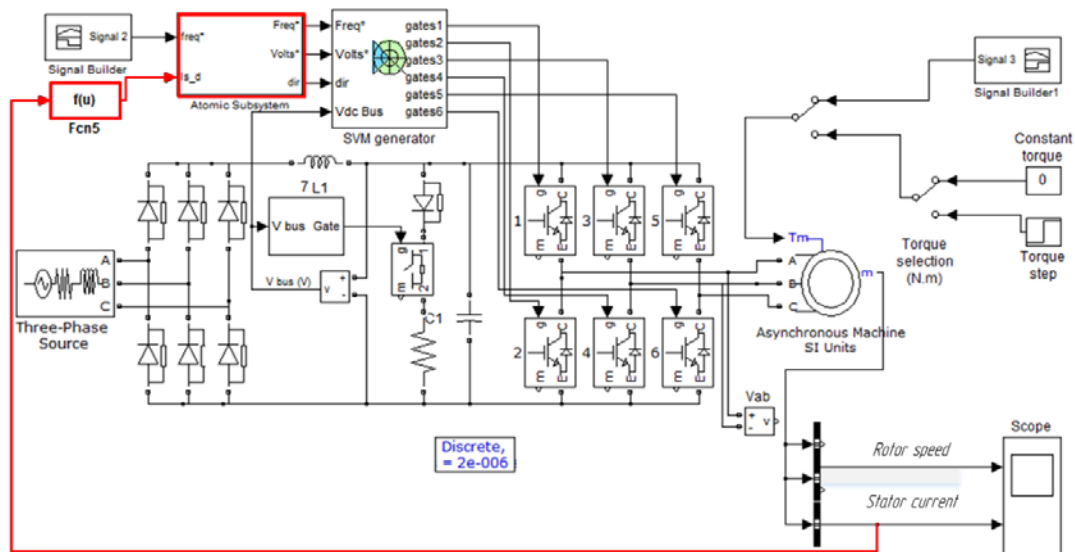


Figure 3. Scheme of a scalar control model with positive feedback

Simulation of processes of sequential acceleration to speeds corresponding to the supply voltage frequency of 10 - 20 - 30 - 40 – 50 Hz was carried out, at each speed of rotation a load was drawn. The angular velocity of the motor shaft and the rms values of the rotor and stator flux linkages and the stator current were controlled. The rms values were calculated from the projections on the d and q axes of the corresponding signals, which are available for measurement in the model of an asynchronous electric motor. The last signal is required to evaluate the efficiency of the drive. The simulation results of scalar control without feedback are shown in Figure 4, of the vector control with a single speed contour (without a flux linkage contour) - in Figure 5 and scalar control with positive feedback on the rms value of the stator current

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and a dynamic link - in Figure 6. At the same time, special attention was paid to the change in the stator and rotor fluxes at the moment of loading. The deviations of the rotor and stator under load from the values at idle for different frequencies of the supply voltage with different control algorithms are shown in Tabel. 1.

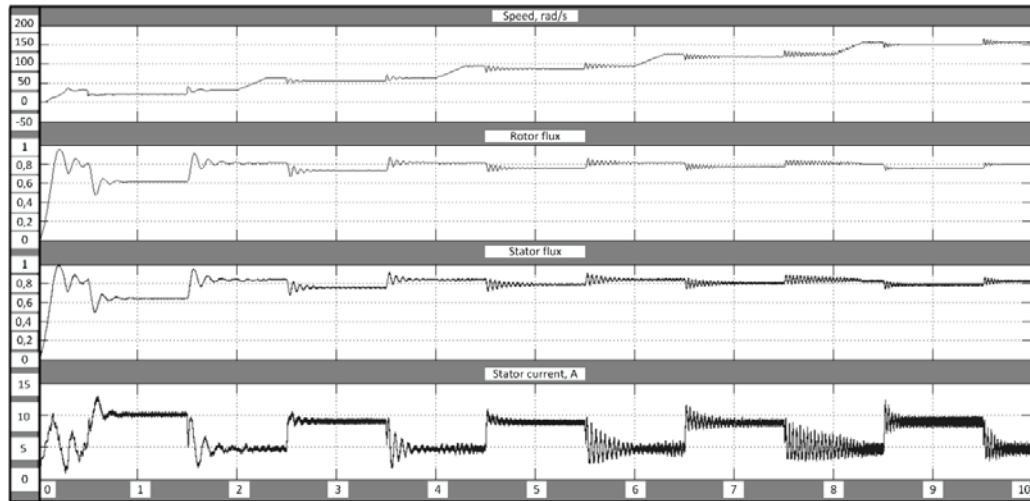


Figure 4. Modelling processes in an asynchronous electric drive with scalar control without feedback

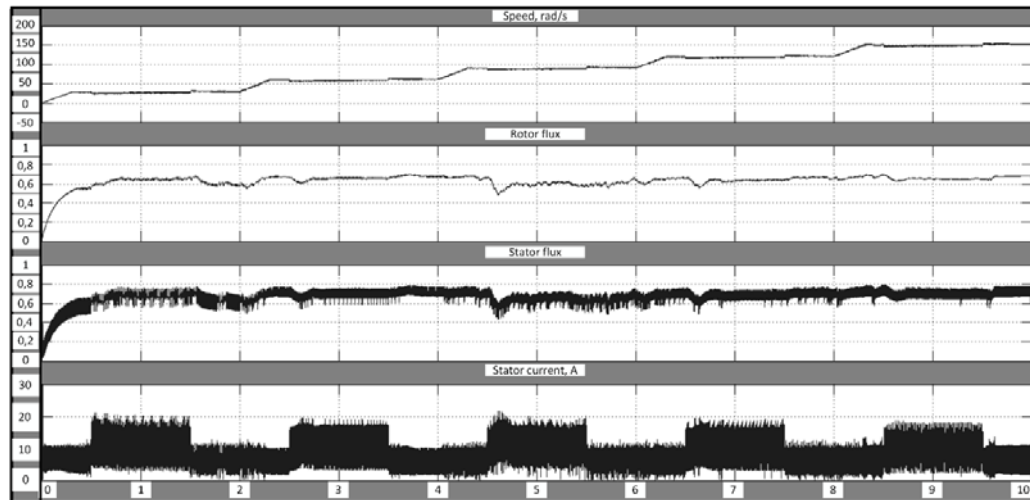


Figure 5. Modelling processes in an asynchronous electric drive with vector control system

Table 1. The deviations values of the rotor and stator flux under load for different frequencies of the supply voltage and control system

Control system	Maximum deviations of rotor / stator fluxes, $V \cdot s$				
	10 Hz	20 Hz	30 Hz	40 Hz	50 Hz
Scalar control without feedback	-0,2/ -0,2	-0,09/ -0,11	-0,05/ -0,05	-0,03/ -0,03	-0,04/ -0,03
Vector control with a single speed contour	0,06/ 0,1	-0,03/ -0,04	-0,05/ -0,06	-0,03/ -0,03	-0,03/ -0,03
Scalar control with DPF	-0,1/ -0,1	-0,03/ -0,03	-0,03/ -0,03	-0,03/ -0,03	-0,04/ -0,02

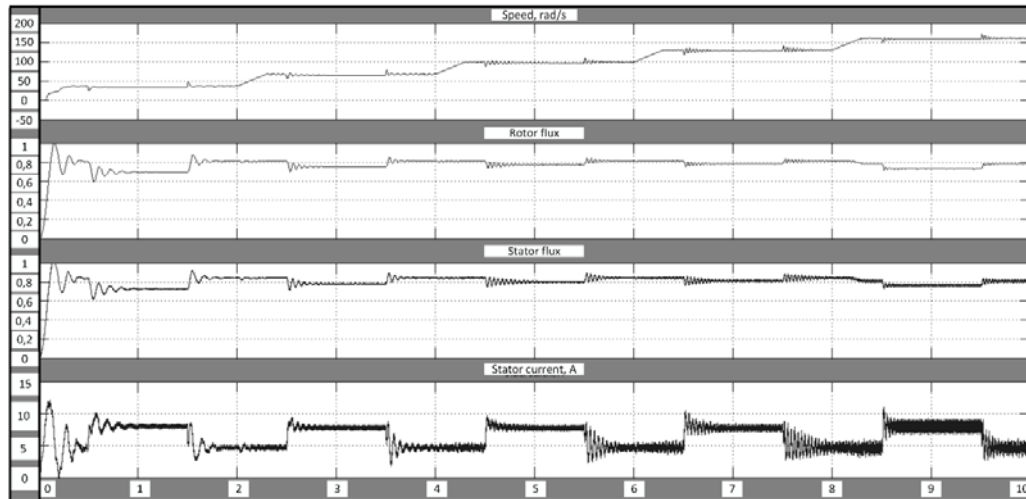


Figure 6. Modelling processes in an asynchronous electric drive with scalar control without feedback

In scalar control, the maximum possible value of standard IR -compensation was established (which maintains stability). At the same time, the scatter of stator and rotor fluxes at low speed (30 rad / s) is in the region of $0,2 \text{ V} \cdot \text{s}$, and decreases to $0,1 \text{ V} \cdot \text{s}$ with an increase in speed to nominal (157 rad / s). With the introduction of the DPF, the flow deviations during accelerations and load surges do not exceed $0,1 \text{ V} \cdot \text{s}$. With vector control, the mean value of the flow deviations is also $0,1 \text{ V} \cdot \text{s}$, but at the same time, there is a high-frequency component in the stator flow. Attention should be paid to the stator currents, which are the greatest in vector control and minimal in DPF Tabel 2. Thus, the simulation clearly showed that in the electric drive with DFT the flow stabilization is practically at the same level as the vector control.

Table 2. The values of stator currents under load for different frequencies of the supply voltage and control system

Control system	Stator current under load, A				
	10 Hz	20 Hz	30 Hz	40 Hz	50 Hz
Scalar control without feedback	10	8	7,5	7,5	9
Vector control with a single speed contour	14	13	12	13	13
Scalar control with DPF	8	7	7	7,5	8,5

In addition, processes in a drive with vector control with a speed error of 2 and 4% are simulated Figure 7, 8. The simulation results are very visual. With the introduction of an error rate of 2% into the signal Figure 7, the control loses operation at a speed corresponding to the frequency of the stator voltage of 40 Hz, and with an error of 4% - 30 Hz Figure 8. Large stator currents are a very serious problem for drives in transport and power complexes, where the load is non-deterministic.

Thus, the modeling of processes with control of flux linkage fully confirmed the assumption of Professor A. Usoltsev, and explained the reason for the significant advantages of the proposed DPF over traditional algorithms. You can implement this correction, without any changes in the circuits and algorithms of standard frequency converters, on a programmable logic controller. This makes the widespread use of the proposed correction available in almost any electric drive. The authors are grateful to the seminar at the National Research University of Information Technologies, Mechanics and Optics, and especially to Professor A. Usoltsev, who is considered the author of the idea of this simulation.

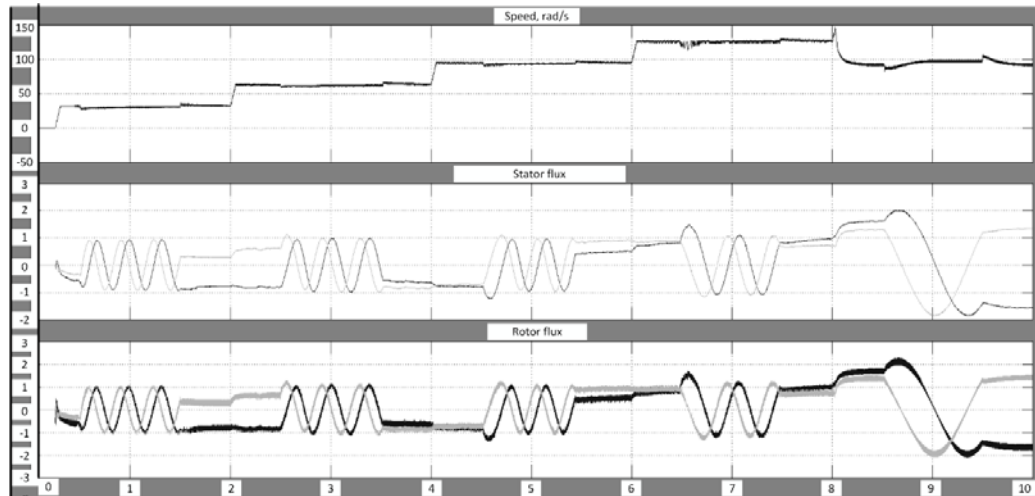


Figure 7. Vector control with speed error of 2%

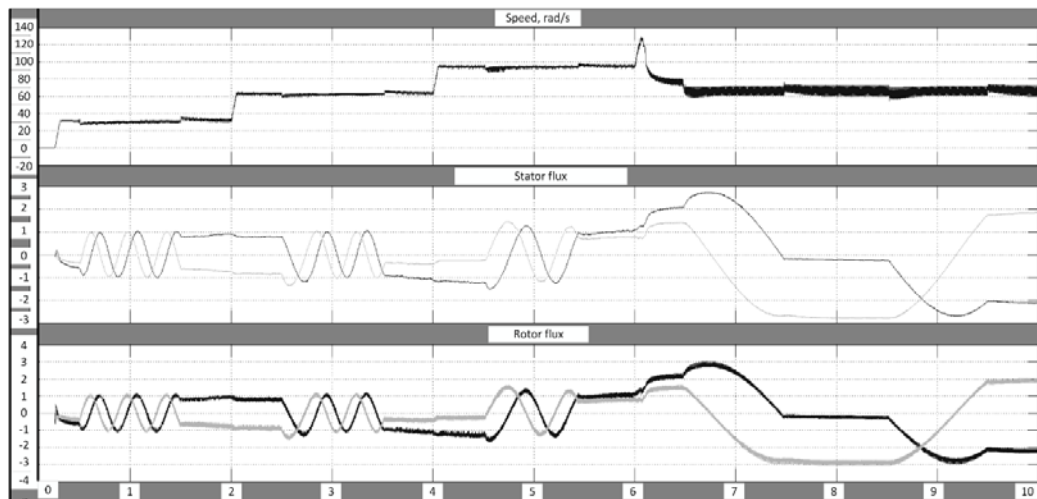


Figure 8. Vector control with speed error of 4%

4. CONCLUSIONS

The conducted simulation of AED FR with scalar control and positive feedback on the stator current showed that this correction allows stabilizing the flux linkage of the rotor and stator in an electric machine. This ensures a more efficient formation of the electromagnetic moment at lower stator currents and less absolute slip. In turn, such a correction improves the static and dynamic characteristics of an asynchronous electric drive with frequency control, and makes it possible to use middle-class technical-economic frequency converters in complex industrial mechanisms with high demands on the static and dynamic characteristics of the drive.

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