Impact of field roughness and power losses, turbulence intensity on electricity production for an onshore wind farm

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ABSTRACT

When designing a power generation project from a different source, and in our case study, wind, when calculating the annual energy produced, it is necessary to define and calculate the losses incurred in the system. The main cause of losses in a wind park is due to the oscillations caused by the turbulence of the air around the turbine because of roughness of terrain. The paper describes two methods of estimating turbulence intensity: one based on the mean and standard deviation (SD) of wind speed from the nacelle anemometer, the other from mean power output and its SD. These analyses are very important for understanding the fatigue and mechanical stress on the wind turbines. Then significance of the site ruggedness index (RIX) and the associated performance indicator (ΔRIX) are confirmed for terrain and the consequences of applying WAsP outside its operating envelope are quantified.

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1. **INTRODUCTION**

The structure, operation, and planning of electric power networks will undergo considerable and rapid changes due to increased global energy consumption. Therefore, electric utility companies are striving to install wind turbines as energy resources to meet growing customer load demand [1, 2]. The mechanical energy from wind after getting converted into electrical energy through turbine and generator, enters into the collector system of the wind farm [3]. Wind turbine technology has undergone a revolution during the last century [4, 5]. Because of excessive investment, climate limitations, and maintenance difficulties of offshore wind farms compared to onshore wind farms, onshore wind farms are also attracting increasing attention from wind power companies [6]. More fundamentally, understanding and reliably predicting wind dynamics remains a central problem in order to forecast wind power [7]. Turbulence in the wind is caused by dissipation of the wind's kinetic energy into thermal energy through the creation and destruction of progressively smaller eddies [8, 9]. To calculate the amount of energy obtained from a turbine located at the aforementioned location, the analytical path is used, recognizing the strength of the wind and the mechanical strength obtained from it [10, 11]. More fundamentally, understanding and reliably predicting wind dynamics remains a central problem in order to forecast wind power [12]. The ruggedness index concept has been used extensively over the last 10 years in wind resource assessment and siting studies in complex terrain, especially in terrain, which is outside the operational envelope of linearised flow models such as WAsP [13]. Kosovo as a signatory of the Energy Community Treaty plans the construction and use of renewable energy capacities in the value of 20%. One of the ways of using renewable energy in Kosovo is the use of wind power [14]. Site ruggedness index calculations have now been implemented in the WAsP program for all predictor and predicted sites [15]. The major goal of Optimal Power Flow (OPF) is to improve a target capacity such as cost of fuel by means of ideal change of the control variables simultaneously different equality and inequality constraints [16, 17].

Wind and other meteorological measurements with a met mast on site starting from August 2017 to December 2017 are made for Kitka Wind Park in Kamenica. This farm is located at about 7km north of Kamenica city of Kosovo, which is at the eastern part of Kosovo.

Based on the correlation coefficient and concurrent measurement period of datasets, 30 – year time series have been synthesized. Regarding uncertainties were taken into account in analysis.

It is noted that measurement period covers only 3.5 months and average wind speed is affected by seasonal variations. As measurement period is coinciding with low wind, season 6% increase in average wind speed is compatible with long-term data trends. First, we will investigate to what extent the site ruggedness index and orographic performance indicator concepts are still supported when using contemporary calculation procedures and topographic data. The study of the field roughness index was done using WAsP software.



Figure 1. Long-term monthly wind speed trends (reference time series)

Table 1. Comparison of wind data measurement			
Long-term Measurement Source	Correlation Coefficient R ²	Period	Wind Speed
	(Weekly Average)		Adjustment
MERRA-2 Reanalysis Data	0.221	01.01.1995 - 21.10.2017	-
MERRA-2 Raw Reanalysis Data	0.694	01.01.1987 - 30.11.2017	105.99%
NCAR - CFSR Reanalysis Series	0.258	01.01.2011 - 30.11.2017	-

2. METHOD OF STUDY

The site consists of agricultural land, short shrubs and forest areas. Most of the wooded areas are on the northern hillside of the site. Wooded areas are showing similar characteristic of about 10m height and closed formation. General Electric 3.6MW and General Electric 3.2MW turbines are studied for the site. Turbines characteristics are given in below table.

Table 2. Technical characteristics of wind turbines taken in study			
Variables	General Electric 3.2MW	General Electric 3.6MW	
Power	3200 KW	3600 KW	
Hub Height	110 m	110 m	
Rotor Diameter	130 m	137 m	
Sweeping Area	53,093 m ²	58,965 m²	
Tower	Tubular	Tubular	
Grid connection	50/60 Hz	50/60 Hz	
IEC Class	IIB (Medium TI)	IIIC (Low TI)	
Power Curve Air Density	1.225 kg/m3	1.225 kg/m3	

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Figure 2. Ce and Ct curves for GE wind turbines, and power curve based on wind speed

Turbulence intensity (TI) is one of the variables to estimate fatigue loads on the turbine components. It is defined as the ratio of the wind speed standard deviation to the wind speed. As the result of expected wind speed increase due to boundary layer wind shear characteristic of the wind, a proportional decrease in turbulence intensity is also expected at upper heights, as in Figure 3 is shown. IEC propose a method to define turbine class according to turbulence intensity at 15m/s wind speed. Average ambient turbulence intensity at met mast location at hub height is obtained as follows.



Figure 3. Changing of wind speed by altitude in study terrain, Kitka

Onshore wind farms: Wind turbines sitting over complex terrains, Atmospheric stability is rarely close to near neutral (highly convective – unstable during the day time and highly stable nocturnal conditions with high shear at night time), much higher ambient turbulence level [18, 19]. The surface flow characteristics are highly dependent on the slope of the hill [20, 21].

Wake effects have been calculated by N.O Jensen Wake model. Park efficiency of 95.4% is achieved. Turbines are not observed to be aligned in prevailing wind direction and in non-prevailing wind direction horizontal distances are considered suitable.



Figure 4. Placement of wind turbines



Figure 5. Wind farm turbines layout and Kitka wind rose

3. RESULTS AND DISCUSSIONS

Vertical extrapolation uncertainty is resulted from two different sources. Difference between measurement height and hub height is one of them and considered as 0.7% per 10m difference in accordance with the complexity of the site. The other source of uncertainty is the difference between elevation of the met mast and the turbines, which is considered 0.7% per 10m elevation difference for the site. Resulting wind speed and annual energy production uncertainties for each turbine is presented below. Due to the high elevation differences between met mast and the turbine T1G higher AEP uncertainty is expected. CFD analysis of the site will substantially reduce these uncertainties. The sensitivity of the flow field to the terrain description has direct consequences for numerical modelling, which is the preferred tool for estimating how the terrain affects wind resources at wind-turbine sites [22, 23].

Table 3. Wind turbines delta elevation and delta height with annual energy production

WTG	Delta elevation	Delta height	Result, wind speed m/s	Result, AEP %
T1	-93.4m	26m	6.8	12.4
T2	-60.0m	26m	4.6	8.5
T3	-20.2m	26m	2.3	4.1
T4	-40.1m	26m	3.3	5.8
T5	-30.0m	26m	2.8	4.9
T6	-0.0m	26m	1.8	3.2
T7	-28.2m	26m	2.7	4.9
T8	10.0m	26m	1.9	3.5
T9	20m	26m	2.3	4.0
T10	-20m	26m	2.3	4.2
		Total		5.6



Figure 6. Annual energy production from wind turbines in Kitka, based on delta elevation of their placement



Figure 7. Comparison between delta elevation and delta height of wind turbines and wind speed on them

The characteristics of the turbines obtained in the study, together with the test conditions under which the test characteristics for the respective power result, are given below.

Table 4:	Technical characteris	tics of two wind turbine	models
_	Turbine type	7 x GE 3.6-137	
_		3 x GE 3.2-130	
	Hub height	110 m	
	Rated power	3600 kW & 3200 kW	
	Number of turbines	10	
	Installed canacity	34.8 MW	

Table 5. Annual energy production from wind farm

Gross annual energy production 122,883 MWh Wake effects 95.4%
Wake effects 95.4%
Availability 06.20/
Availability 90.5%
Turbine Performance 99.7%
Electrical losses 98.0%
Environmental losses 98.5%
Curtailment losses 100.0%
Total Losses 88.4%

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Tables 6 and 7, shows the results of calculations of the mean value of turbulence intensity at different measuring heights during the one-year measurement period. Only ten-minute intervals were considered where the wind speed was higher than 3 m/s.

Table 6. Average value of wind turbulence intensity in Koznica wind park, for different measuring heights,

during the measureme	ent period dur	ing one year (v	w ≥3 m / s)
Height of measurement	84m	60m	40m
TI(w=3m/s) (%)	10.5	10.9	11.4

Table 7. Average value of wind turbulence intensity in Koznica wind park, for different measuring heights, during the measurement period during one year ($w \ge 15 \text{ m/s}$)

8	0		
Height of measurement	84m	60m	40m
TI(w=15m/s) (%)	13.79	14.3	14.34

It is extremely valuable – and sometimes required for bankable estimates – to install two or more masts at the wind farm site; cross-prediction between such masts will provide assessments of the accuracy and uncertainty of the flow modelling over the site. Two or more masts are also required in complex terrain, where ruggedness index (RIX) and Δ RIX analyses are necessary, as in figures 8 and 9, where RIX characteristic is a very important point [24, 25].



Figure 8. Reference site and WT RIX, and difference between them



Figure 9. Comparison of reference site roughness based on wind turbine number and based on their elevation

As expected in this case, from the figures presented in Figure 9, the roughness of the terrain is unchanged and less than that of the wind turbines, while the dRIX in the wind turbines increases this value because of additional turbulence created in them.

4. CONCLUSIONS

Kitka has a moderate wind resource for wind power development. Wind behavior at the met tower sites demonstrates low extreme wind probability but moderately high-to-high turbulence due to heavy brush to the north. From the above analysis it can be clearly seen how the relationship between RIX of site and RIX of wind turbines. The roughness index for the case of the ground surface where the wind turbines are located is constant no matter how the altitude of the terrain changes where they are located within the wind park. As Δ RIX values between met mast and turbine locations are in the range of 2.2% and 7.8%, similarity principle can be said to be mostly achieved. Since the degree of roughness of the turbines depending on the terrain where they are to be located is within the accepted range then it follows that similar turbines can be installed in Kitke without prejudice to the quality of energy that can be produced.

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