

An interleaved DC charging solar system for electric vehicle

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ABSTRACT

This paper investigates the performance of conventional boost converter, 2-phase interleaved boost converter and 3-phase interleaved boost converter for renewable energy applications especially for solar-powered energy. The advantages of using coupled inductors in interleaved boost converters include increased system efficiency, reduced core size, and also reduced overall current and voltage ripples which increases the lifetime of renewable energy resources. In this paper, the uses of boost converters have been focused explicitly on the interleaved DC-DC charging from a solar-powered battery into electric vehicle (EV) battery storage. Hence, this paper aims to investigate a suitable charging process mechanism from a photovoltaic (PV) battery storage system into EV powered battery system. Using the application of a boost converter with reduced ripple current and ripple voltage decreases switching losses and increases conversion efficiency. The simulation is carried out by using Simulink/MATLAB to evaluate the performance of each boost converter. The results successfully demonstrate the ability of the proposed charging system with an energy efficiency of 90%.

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1. INTRODUCTION

The transportation sector is recognized as the main contributor to the worrisome effect of the green house gases (GHG) and thus, the electric vehicle (EV) technology is regarded as one of the prominent solutions towards the reduction of this problem [1], [2]. In EV technology, the vehicle relies on the battery instead of fuel as the energy supply for its system operation. Due to the limited and constrain power available in the battery for the EV, various studies have been conducted to prolong the battery life and maximizing the EV potential for long-run operation [3], [4]. The research on the EV system is not only limited to the components and control strategy in the EV system itself, the charging strategy is also another means towards the improvement of the EV for sustainability in the transportation sector [5], [6].

Nowadays, being able to charge the EV can mean the difference between hours of care-free use or scrambling to find the nearest power outlet. The issue of electrical burden has been raised during the peak demand duration and requires methods to overcome the drawbacks [7]-[9]. The impact of charging the EV

transportation networks influenced directly the generation, transmission and distribution of power grids [10], [11]. An OFF-grid or the standalone charging system emerged as the best option for electrification as it eliminates the need for the connection to the charging utility such as the requirements for the transmission and distribution on the power grid [12]. Moreover, it is very well suitable to meet the power need especially in remote areas as it relies on renewable energy resources [13], [14]. Renewable energy comes from many commonly known sources such as solar power, wind, water and geothermal.

The idea of a solar charging system seizes researchers' attention to provide a solution for power crisis issues while suggesting a clean, economical, and sustainable power source for an electric vehicle. However, many issues have been raised when the proposed application of high power charging system solely depending on only solar energy system [15]. Specifically, for solar-powered energy, a combination of photovoltaic (PV) with the power grid system and PV-Standalone Charger are an excellent method that has been proposed [16]-[18]. Both of them require a suitable converter to make it more efficient since the conversion efficiency of the PV array is very small compared to the battery storage capacity [19]-[21]. A conventional boost converter is one such converter that can be optimized for these applications.

Hence, this paper aims to investigate a suitable charging process mechanism from the PV battery storage system into EV powered battery system. Using the application of a boost converter with reduced ripple current and ripple voltage decreases switching losses and increases conversion efficiency. By implementing a boost converter, all goals can be achieved except for line and load regulations since it only can be improved by using the higher quality capacitors so that it can hold up the voltage better on the circuit board [22]. By using the interleaving method, also called multi-phasing, which requires a parallel combination of multiple sets of switches, diodes and inductors connected to a single capacitor, it can effectively reduce the size of the filter components while exhibits lower output current and voltage ripples [23], [24]. Theoretically, interleaving methods can cover the losses due to the phase shift of 180 degrees ripple cancellation takes place [25].

The remainder of this paper is organized as shown in. The background of the study of this paper is introduced in section 1. While the details of the operation for each converter namely; conventional boost converter, 2-phase interleaved boost converter (IBC) and 3-phase interleaved boost converter are described in section 2 and the simulation of the PV characteristics is described in section 3. The selection of the suitable charging mechanism is elaborated in section 4. Finally, the paper is concluded with findings from the analysis in section 5.

2. METHODOLOGY

In this paper, three types of topologies for the DC-DC converter charging system are studied and investigated namely; the conventional boost converter, 2-phase interleaved boost converter and 3-phase interleaved boost converter. The higher output voltage can be produced when using the large inductor that is connected in series with the power supply. When the switch is on, the inductor gets charged by the supply, and when the switch is off, both the supply and the inductor will give supply to the load and act as the transformers from DC to DC. Even though it has many advantages, its application is limited due to the ripple current and voltage. Ripples are wasted power and have many undesirable effects in a DC circuit such as it heats the components, affecting the digital circuits to operate improperly and also contributes to noise and distortion. The ripple can be reduced by an electronic filter and some can be eliminated by using a voltage regulator [26].

2.1. Duty ratio, D

Duty cycle, D of the proposed charger can be expressed as shown in (1).

$$D = 1 - \frac{V_{in} \times \eta}{V_{out}} \quad (1)$$

Where V_{out} is the output voltage, V_{in} is the input voltage, and η is the efficiency of the converter.

2.2. Inductor, L

The inductor, L can be expressed as shown in (2).

$$L = \frac{V_{in}(V_{out}-V_{in})}{\Delta I_L * f_s * V_{out}} \quad (2)$$

where f_s and ΔI_L are the minimum switching frequency of the converter and estimated inductor current ripple respectively. For the ΔI_L , a good estimation for the inductor ripple current is 20% to 40% of the output

current. Theoretically, a smaller ripple current reduces the magnetic hysteresis losses in the inductor, as well as output voltage ripple. The formula can be found out as shown in (3).

$$\Delta I_L = (0.2 \text{ to } 0.4) * I_{out(max)} * \frac{V_{out}}{V_{in}} \quad (3)$$

Where $I_{out(max)}$ is the maximum output current desired in the application. After calculating the value of inductance L, we can verify the value of inductor ripple current ΔI_L using (4).

$$\Delta I_L = \frac{V_{in(min)} * D}{f_s * L} \quad (4)$$

2.3. Capacitor, C

In the proposed charger, capacitor C resonated with inductor L to smoothen out switch voltage at turn-off transition. Thus, the suitable energy to be stored in C can be determined as 5.

$$C_{out(min)} = \frac{I_{out(max)} * D}{f_s * \Delta V_{out}} \quad (5)$$

where $C_{out(min)}$ and $I_{out(max)}$ are the minimum output capacitance needed and maximum output current of the desired application respectively. While ΔV_{out} is the desired output voltage ripple.

2.3. Resistance, R

Interleaving also can be known as multi-phase is a developed technique to overcome the conventional boost converter disadvantages. It is a useful technique to reduce the size of filter components by setting the components into a parallel combination of a set of two switches, diodes, and inductor that is connected to a single capacitor and load. The load or resistance, R, value can be calculated using (6).

$$R = \frac{V_{out}}{I_{out}} \quad (6)$$

3. PV CHARACTERISTIC

For the solar characteristic, there are many types of PV modeling methods available, and one of them is the single diode model of the PV Module. By using SIMSCAPE and Simulink software, the simulation is conducted to determine the relationship between the variation of irradiance and temperature level with the output power produced. The characteristic of the PV panel applied in this study is listed in Table 1. Several irradiance levels are tested for the test which include 600 W/m², 700 W/m², 800 W/m², 900 W/m², and 1000 W/m² with a constant temperature of 25°C. Based on the plotted graph on Figure 1 (a), the reduction of irradiance will affect the output power of PV panel and changing its maximum power point (MPP) position. The power axis range is from 1.957 V to 3.396 V for irradiance variation from 600 W/m² to 1000 W/m².

Since irradiance with 1000 W/m² will provide the highest MPP value, the model is tested with a different value of temperature including 10° C, 20° C, 30° C, 40° C, and 50° C with a constant irradiance of 1000 W/m². Figure 1 (b) portrays the P-V characteristics on a different level of temperature. Similar to Irradiance variation, temperature changes also will affect the output power of the PV panel while changing its MPP position. The Power axis range from 3.339 W to 3.431 W for temperature range 10° C to 50° C. It is known that the conversion efficiency of the PV array is very small compared to the battery capacity [27], [28]. Thus, to increase efficiency, high-energy processors are required. Transformers is not suitable for this project because transformers can only step up AC-AC but this scope of study only covers a stand-alone off-grid system. Hence, this project mainly adopts a DC-DC converter to increase the voltage to the desired amount using the boost converter.

Table 1. Specification of PV panel

Parameter	Value
Open Circuit Voltage (V_{oc})	48
Short Circuit Current (I_{sc})	9.2
Quality Factor	1.5
Series Cell	1
Energy Gap	1.11

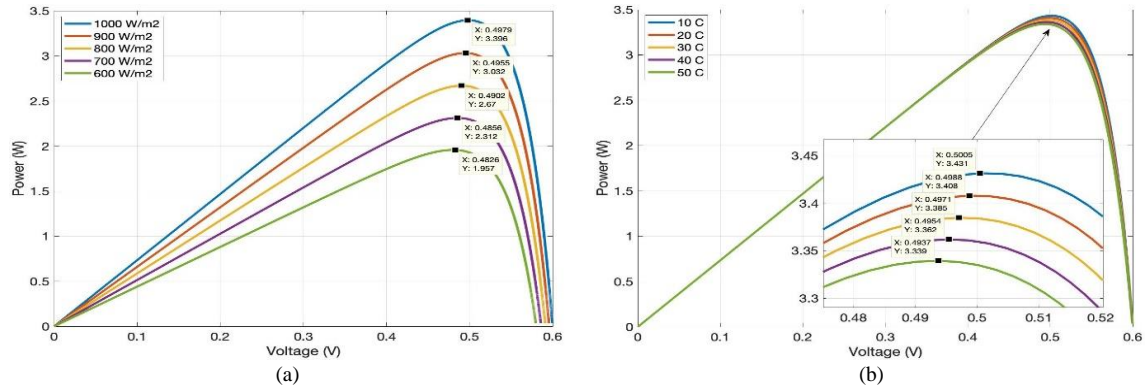


Figure 1. Input waveforms of PV curve depending on; (a) the irradiance level and (b) the temperature level

4. RESULT AND DISCUSSION

The analysis from the simulation is explained in terms of the efficiency of the converters, the reduction of values of ripple and the transition time from the transient state into the steady state in the system design that has been developed earlier. For the simulation of the conventional boost converter, the inputs to the system are demonstrated by Figure 2 (a) and (b). As mentioned earlier, the current that goes into the inductor is similar to the input current are shown in Figure 2 (a). They can be obtained as 10.39 A, and by using the same waveform, the input current ripple is obtained as 2.35 A. And Figure 2 (b) shows the gating pattern of MOSFET.

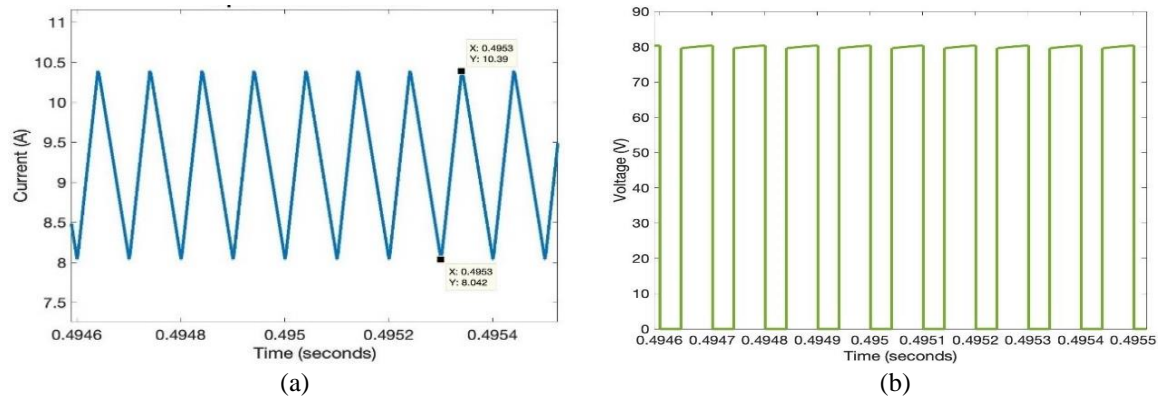


Figure 2. Input waveforms of conventional boost converter; (a) current and (b) gating pattern of MOSFET

For the 2-phase interleaved boost converter, Figure 3 (a) shows the input current waveform, inductor L1 and inductor L2 current waveforms with the values of 9.936 A and 3.469 A respectively. Using the same waveform, the input current ripple is accumulated as 0.76 A, and both inductor current ripples are 2.35 A, similar to the conventional boost converter. The gating pattern of MOSFET M1 and MOSFET M2 of 2-Phase interleaved boost converter is shown in Figure 3 (b). In the simulation of 3-phase interleaved boost converter, the input current, inductor currents (L1, L2, and L3) are shown in Figure 4 (a) and are detected at 9.019 A and 4.315 A respectively. Meanwhile, the input current ripple is obtained at 0.52 A and all inductor current ripples are at the value of 2.35 A, the same value detected in conventional boost converter and 2-phase interleaved boost converter. The switching patterns of three MOSFETs M1, M2, and M3 in the 3-phase interleaved boost converter can be demonstrated in Figure 4 (b). The phase shift is recorded at 120 degrees ($360/n$ where n is 3).

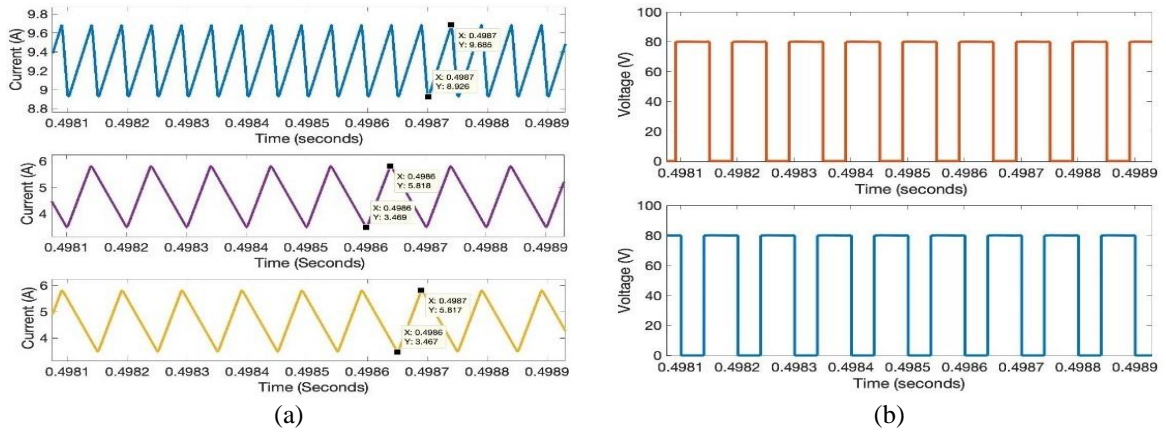


Figure 3. Waveform of the 2-phase interleaved boost converter (a) input current and (b) gating pattern of MOSFET

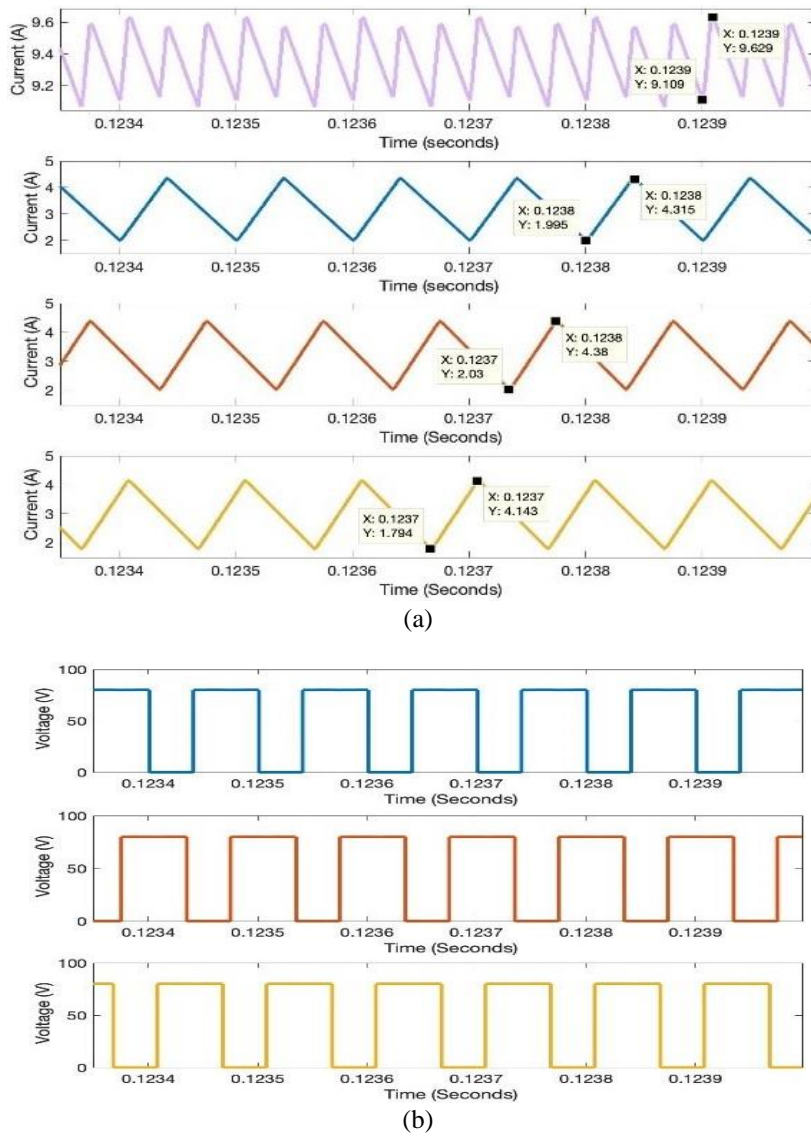


Figure 4. Waveform of the 3-phase interleaved boost converter (a) input current and (b) gating pattern of MOSFET

4.1. Comparative analysis

Based on Figure 5 (a) and (b), the conventional boost converter produced the output current and output voltage of 5.523 A and 79.54 V respectively. The output current ripple can be calculated from the same figure and is calculated at the value of 0.79 V. Thus, the efficiency of the conventional boost converter is only up to 88.09%. However, the transient response of the system for the conventional boost converter shows that a longer setting time is needed for this type of converter as shown in Figure 6. Moreover, the conventional boost converter simulation results do not produce the expected result, to run efficiently in stepping up the voltage level. So, to overcome the drawbacks, the idea of having an interleaved boost converter is applied.

When the system is applied with the 2-phase interleaved boost converter, the output current is detected at 5.503 A and the output voltage is at 79.25 V. Thus, the efficiency of a 2-phase interleaved boost converter is 91.44% which is better than a conventional boost converter. The output current ripple for the 2-phase interleaved boost converter can be observed in Figure 5(a) and Figure 5(b) at 0.046 A, with the output voltage ripple is 0.14 V. In terms of the transient response in Figure 6, the 2-phase interleaved boost converter exhibits a much better and faster response in comparison to the conventional boost converter but with slightly slower than the 3-phase interleaved boost converter.

When the system is applied with the 3-phase interleaved boost converter, the output current is detected at 5.501 A while output voltage is at 79.21 V as demonstrated in Figure 5. Hence, the efficiency becomes 99.66% which makes the 3-phase interleaved boost converter has the highest efficiency among all tested converters in this study. The output current ripple is calculated at 0.004 A and the output voltage ripple is also shown in Figure 5 with a value of 0.060 V. It can be inferred from the Figure 5, that when the interleaved methods are applied, the ripple will be reduced significantly.

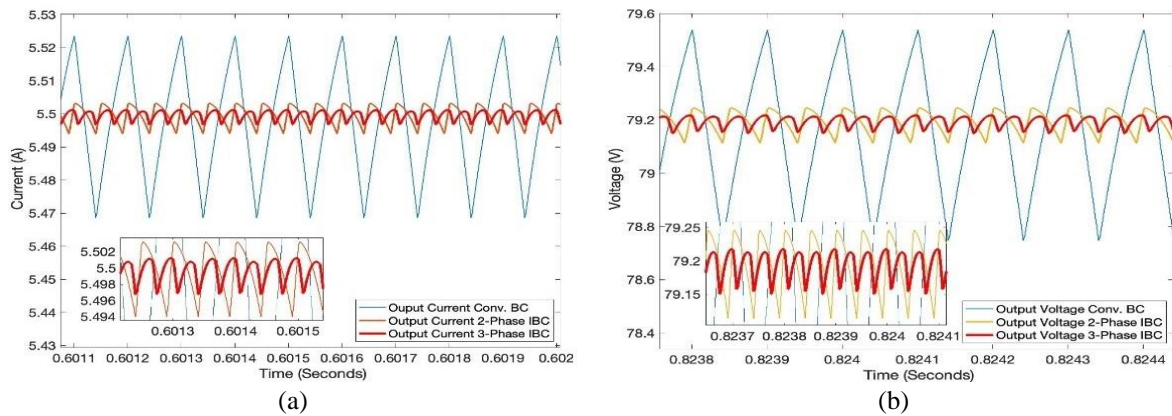


Figure 5. Output waveforms of the conventional boost converter, (a) current, (b) voltage

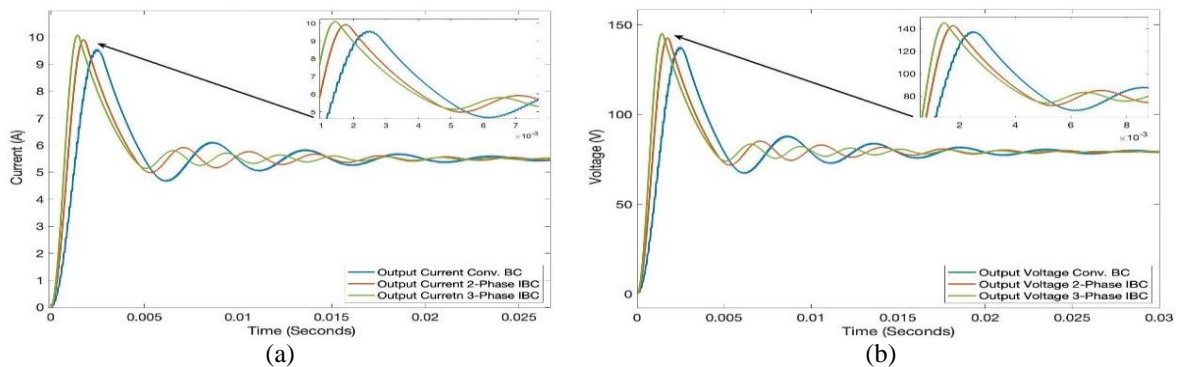


Figure 6. Transient-steady state of output waveforms, (a) current, (b) voltage

Furthermore, Figure 6 (a) shows the time taken for the current to change from a transient state into a steady state. Between those three boost converters, 3-phase interleaved boost converter shows the fastest

transition compared to the other two. Similarly, Figure 6 (b) shows the time taken for the voltage to change from a transient state into a steady-state, 3-Phase interleaved boost converter also leads to the transition process. Table 2 summarises the complete comparisons between conventional boost converter, 2-phase interleaved boost converter, and 3-phase interleaved boost converter.

Table 2. Comparison of boost converters

Parameters	Conventional Boost Converter	2-Phase Interleaved Boost Converter	3-Phase Interleaved Boost Converter
Input Voltage	48V	48V	48V
Input Current	10.39A	9.936A	9.109A
Input Power	498.72W	476.928W	437.232W
Output Voltage	79.54V	79.25V	79.21V
Output Current	5.523A	5.503A	5.501A
Output Power	439.3W	436.113W	435.73W
Efficiency	88.09%	91.44%	99.66%
Duty Ratio	0.4	0.4	0.4
Switching Frequency	10kHz	10kHz	10kHz
Inductor Current Ripple	2.35A	2.35A	2.35A
Output Current Ripple	0.054A	0.046A	0.004A
Output Voltage Ripple	0.79V	0.14V	0.060V

5. CONCLUSION

This paper aims to investigate a suitable charging process mechanism from a Photovoltaic (PV) battery storage system into EV powered battery system. Using the application of a boost converter with reduced ripple current and ripple voltage decreases switching losses and increases conversion efficiency. The effect of a coupled inductors on both the inductor current ripple, the output current ripple, and the output voltage ripple is studied in great detail. The major contributions of the paper are summarized as; To investigate suitable charging process mechanism from PV battery storage system into EV powered battery system; To design and develop an interleaved boost converter with a reduction of ripple current and voltage to decrease switching losses and increase conversion efficiency; To evaluate the performance of the interleaved boost converter as the DC-DC Charging System between PV battery storage system and EV powered system. From the analysis, it is shown that the output current ripple is reduced from 0.054 A in conventional boost converter into 0.046 A in 2-phase interleaved boost converter and 0.004 A in 3-phase interleaved boost converter. The output voltage ripple also is reduced from 0.79 V in conventional boost converter to 0.14 V in 2-phase interleaved boost converter and 0.06 V in 3-phase interleaved boost converter. Thus, it justified that the leakage inductance could be prevented by increasing the switching patterns to minimize the output Current and voltage ripples. Furthermore, the 3-phase interleaved boost converter also has the fastest transition from a transient state into a steady-state compared to 2-phase interleaved boost converter and conventional boost converter. Additionally, the simulation results, validate that 3-phase interleaved boost converter has higher efficiency than a 2-phase interleaved boost converter. Therefore, a 3-phase interleaved boost converter is proven to be a suitable candidate for DC-DC charging system for renewable energy resources specifically in the electric vehicle application.

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